

## 15.8 Stokes' Theorem

Recall how Green's Theorem could be written

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_D (\nabla \times \mathbf{F}) \cdot \mathbf{k} dA \quad (*)$$

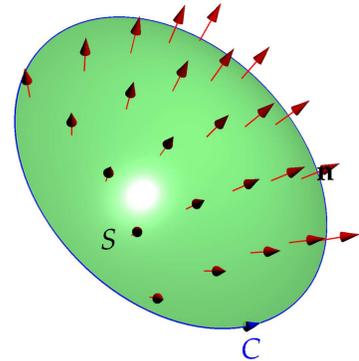
where  $\mathbf{F} = P\mathbf{i} + Q\mathbf{j} + 0\mathbf{k}$  and  $C$  is a simple closed curve in the plane  $z = 0$  with interior  $D$ . Stokes' Theorem generalizes this to a curve which forms the boundary a surface in three dimensions.

To properly discuss this, we need to orient two types of objects:

**Curves** Orientation means the **direction of travel** along  $C$ .

**Surfaces** Orientation means the **direction of the normal vector field**  $\mathbf{n}$ .

As pictured, both orientations can be made compatible in accordance with the right hand rule: curl the fingers of your right hand round  $C$  and your thumb will point (roughly) in the  $\mathbf{n}$ -direction. We can also refer to the orientation *induced* on the (say) the boundary if this is compatible with the orientation of the surface.



**Theorem (Stokes).** Let  $S$  be an oriented piecewise smooth surface with unit normal field  $\mathbf{n}$  and piecewise smooth boundary curve  $C = \partial S$  endowed with the induced orientation. Let  $\mathbf{F}$  be a vector field with continuous partial derivatives on some open region containing  $S$ . Then

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \iint_S (\nabla \times \mathbf{F}) \cdot d\mathbf{S}$$

In two dimensions, a region  $D$  can be thought of a surface oriented upwards ( $d\mathbf{S} = \mathbf{k} dA$ ); the induced orientation on its boundary  $C$  is counter-clockwise, recovering Green's Theorem (\*).

**Example 1** Compute the flux integral  $\iint_S \nabla \times \mathbf{F} \cdot d\mathbf{S}$ , where  $S$  is the part of the paraboloid  $z = x^2 + y^2$  inside the cylinder  $x^2 + y^2 = 4$  oriented upward, and  $\mathbf{F}(x, y, z) = x^2z^2\mathbf{i} + y^2z^2\mathbf{j} + xyz\mathbf{k}$ .

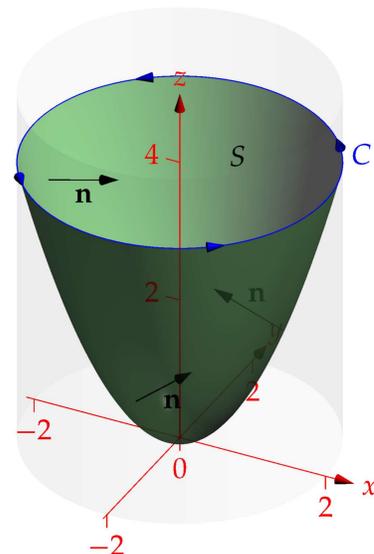
Evaluating the flux integral directly is nasty, so we instead apply Stokes' Theorem.

The boundary curve of  $S$  is the circle  $C$  of radius 2 in the plane  $z = 4$ . Parametrize this by

$$\mathbf{r}(t) = 2 \cos t \mathbf{i} + 2 \sin t \mathbf{j} + 4 \mathbf{k}, \quad 0 \leq t \leq 2\pi$$

Note that the counter-clockwise orientation of  $C$  is induced from the upward orientation of  $S$ . Now compute:

$$\begin{aligned} \iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} &= \int_C \mathbf{F} \cdot d\mathbf{r} = \int_0^{2\pi} \begin{pmatrix} 64 \cos^2 t \\ 64 \sin^2 t \\ 16 \sin t \cos t \end{pmatrix} \cdot \begin{pmatrix} -2 \sin t \\ 2 \cos t \\ 0 \end{pmatrix} dt \\ &= \int_0^{2\pi} 128(\cos t \sin^2 t - \sin t \cos^2 t) dt \\ &= \frac{128}{3} (\sin^3 t + \cos^3 t) \Big|_0^{2\pi} = 0 \end{aligned}$$



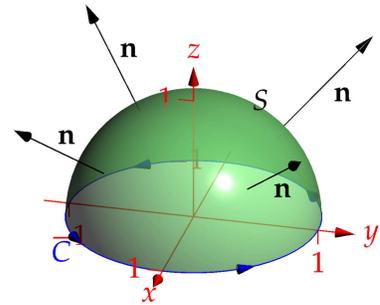
**Example 2** This time we check Stokes' Theorem directly. Let  $S$  be the unit hemisphere with  $z \geq 0$  and  $\mathbf{F} = 2x\mathbf{i} + (x - y^2)\mathbf{j} + xz^2\mathbf{k}$ .

The boundary curve is the unit circle oriented counter-clockwise when viewed from above:

$$\mathbf{r}_C(t) = \cos t \mathbf{i} + \sin t \mathbf{j}, \quad 0 \leq t \leq 2\pi$$

We therefore have

$$\begin{aligned} \int_C \mathbf{F} \cdot d\mathbf{r} &= \int_0^{2\pi} \begin{pmatrix} 2\cos t \\ \cos t - \sin^2 t \\ 0 \end{pmatrix} \cdot \begin{pmatrix} -\sin t \\ \cos t \\ 0 \end{pmatrix} dt \\ &= \int_0^{2\pi} -2\sin t \cos t + \cos^2 t - \cos t \sin^2 t dt = \pi \end{aligned}$$



We can parametrize the surface in several ways to compute the flux integral, though it is helpful here first to observe that  $\mathbf{n} = x\mathbf{i} + y\mathbf{j} + z\mathbf{k}$  on this surface, so

$$\iint_S (\nabla \times \mathbf{F}) \cdot d\mathbf{S} = \iint_S \begin{pmatrix} 0 \\ -z^2 \\ 1 \end{pmatrix} \cdot \begin{pmatrix} x \\ y \\ z \end{pmatrix} dS = \iint_S z - yz^2 dS = \iint_S z dS$$

We used the fact that  $yz^2$  is an *odd function* on the surface. At this point we can parametrize however we like. Using spherical polar co-ordinates,  $dS = \sin \phi d\phi d\theta$  and

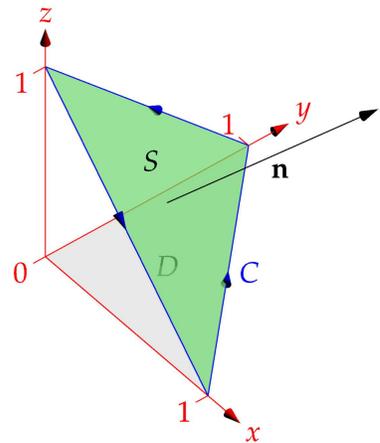
$$\iint_S z dS = \int_0^{2\pi} \int_0^{\pi/2} \cos \phi \sin \phi d\phi d\theta = 2\pi \cdot \frac{1}{2} \sin^2 \phi \Big|_0^{\pi/2} = \pi$$

**Example 3: Choosing the Surface** If Stokes' Theorem is used to help evaluate  $\int_C \mathbf{F} \cdot d\mathbf{r}$  round a closed curve, remember that we can choose *any* surface  $S$  whose boundary is  $C$ !

If  $C$  is the triangle with corners  $(1, 0, 0)$ ,  $(0, 1, 0)$  and  $(0, 0, 1)$  traced counter-clockwise when viewed from above, it seems sensible to *choose*  $S$  to be the plane  $x + y + z = 1$  bounded by  $C$ .

Given  $\mathbf{F} = (x + y^2)\mathbf{i} + (y + z^2)\mathbf{j} + (z + x^2)\mathbf{k}$ , then

$$\begin{aligned} \int_C \mathbf{F} \cdot d\mathbf{r} &= \iint_S \nabla \times \mathbf{F} \cdot d\mathbf{S} = \iint_S \begin{pmatrix} -2z \\ -2x \\ -2y \end{pmatrix} \cdot d\mathbf{S} \\ &= \iint_D \begin{pmatrix} -2(1-x-y) \\ -2x \\ -2y \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} dx dy \\ &= -2 \iint_D dx dy = -1 \end{aligned}$$



where we parametrized  $S$  using standard rectangular co-ordinates, and  $D$  is the base triangle  $0 \leq x \leq 1, 0 \leq y \leq 1 - x$ .

We could have chosen another surface  $S$  with boundary  $C$ : for instance  $S = S_1 \cup S_2 \cup S_3$  as the union of three triangles in the co-ordinate planes  $x = 0, y = 0, z = 0$ , all oriented positively. You should check in this case that the resulting flux integral is unchanged:

$$\iint_S \nabla \times \mathbf{F} \cdot d\mathbf{S} = \iint_{x=0} -2z dy dz + \iint_{y=0} -2x dx dz + \iint_{z=0} -2y dx dy = -\frac{1}{3} - \frac{1}{3} - \frac{1}{3} = -1$$

## Proving Stokes' Theorem

The conceptual part of the proof is little more than an application of Green's Theorem. The nasty part is checking all the algebra...

*Sketch Proof.* Let  $\mathbf{r}(u, v)$  parametrize  $S$  with oriented co-ordinates, where  $(u, v) \in D$ . Let  $\partial D$  be the boundary curve of  $D$  oriented counter-clockwise. Then  $\mathbf{r}(\partial D) = C$ , and the orientations of these curves is compatible. Now compute:

$$\begin{aligned} \int_C \mathbf{F} \cdot d\mathbf{r} &= \int_{\partial D} \mathbf{F} \cdot (\mathbf{r}_u du + \mathbf{r}_v dv) = \int_{\partial D} (\mathbf{F} \cdot \mathbf{r}_u) du + (\mathbf{F} \cdot \mathbf{r}_v) dv \\ &= \iint_D \frac{\partial}{\partial u} (\mathbf{F} \cdot \mathbf{r}_v) - \frac{\partial}{\partial v} (\mathbf{F} \cdot \mathbf{r}_u) du dv && \text{(Green's Theorem on } D) \\ &= \iint_D \mathbf{F}_u \cdot \mathbf{r}_v - \mathbf{F}_v \cdot \mathbf{r}_u du dv && \text{(since } \mathbf{r}_{vu} = \mathbf{r}_{uv}) \\ &= \iint_D \begin{pmatrix} P_u \\ Q_u \\ R_u \end{pmatrix} \cdot \begin{pmatrix} x_v \\ y_v \\ z_v \end{pmatrix} - \begin{pmatrix} P_v \\ Q_v \\ R_v \end{pmatrix} \cdot \begin{pmatrix} x_u \\ y_u \\ z_u \end{pmatrix} du dv && (*) \end{aligned}$$

Now compute from the other side:

$$\begin{aligned} \iint_S \nabla \times \mathbf{F} \cdot d\mathbf{S} &= \iint_D (\nabla \times \mathbf{F}) \cdot (\mathbf{r}_u \times \mathbf{r}_v) du dv = \iint_D \left[ \begin{pmatrix} \frac{\partial}{\partial x} \\ \frac{\partial}{\partial y} \\ \frac{\partial}{\partial z} \end{pmatrix} \times \begin{pmatrix} P \\ Q \\ R \end{pmatrix} \right] \cdot \left[ \begin{pmatrix} x_u \\ y_u \\ z_u \end{pmatrix} \times \begin{pmatrix} x_v \\ y_v \\ z_v \end{pmatrix} \right] du dv \\ &= \iint_D \begin{pmatrix} R_y - Q_z \\ P_z - R_x \\ Q_x - P_y \end{pmatrix} \cdot \begin{pmatrix} y_u z_v - y_v z_u \\ z_u x_v - z_v x_u \\ x_u y_v - x_v y_u \end{pmatrix} du dv \end{aligned}$$

After dotting out and applying the chain rule ( $P_u = P_x x_u + P_y y_u + P_z z_u$ , etc.) to (\*), the two integrands are seen to be equal.

If  $S$  cannot be covered by a single parametrization, then a cut-and-paste argument similar to the proof of Green's Theorem can be used. ■

## Stokes' Theorem and Conservative Vector Fields

Recall that every conservative vector field is irrotational:

$$\mathbf{F} = \nabla f \implies \nabla \times \mathbf{F} = \nabla \times \nabla f = \mathbf{0}$$

As previously advertised, Stokes' Theorem allows us to reverse this, provided the domain is simply-connected. As a loose justification, if  $C$  is any simple closed curve in the domain, let  $S$  be a surface whose boundary is  $C$ , then

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{F} \cdot d\mathbf{S} = 0$$

To see why simple-connectedness is necessary, revisit the rotational example where  $\mathbf{F} = \frac{1}{x^2 + y^2} \begin{pmatrix} -y \\ x \\ 0 \end{pmatrix}$ , whose domain is  $\mathbb{R}^3$  with the  $z$ -axis removed. This has  $\text{curl } \mathbf{F} = \mathbf{0}$ , but is non-conservative. Stokes' Theorem does not apply here since any surface with boundary  $C$  is necessarily cut by the  $z$ -axis.

## Interpreting Curl: Circulation and Local Rotation

If  $C$  is a simple closed curve, the line integral

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C \mathbf{F} \cdot \mathbf{T} ds$$

is also known as the *circulation* of  $\mathbf{F}$  around  $C$ , since we are essentially computing the net component of  $\mathbf{F}$  pointing in the direction of travel round the curve (in the direction of the unit tangent vector  $\mathbf{T}$ ).

Stokes' Theorem lets us interpret the circulation round  $C$  in terms of the curl of  $\mathbf{F}$ : if  $S$  is *any* (suitable) surface with boundary  $C$ , then the circulation equals the flux integral of the curl,

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \iint_S (\nabla \times \mathbf{F}) \cdot d\mathbf{S}$$

Otherwise said, the circulation of  $\mathbf{F}$  around the boundary is the net effect of all the infinitesimal rotations induced by  $\mathbf{F}$  on the surface. But what are these "infinitesimal rotations?" We mentioned this when first discussing curl, but we can now provide some justification.

Let  $S_a$  be the disk of radius  $a$  centered at  $P$  with unit normal vector  $\mathbf{n}$ , and  $\mathbf{F}$  a vector field satisfying Stokes' Theorem. Considering average values,

$$\int_{C_a} \mathbf{F} \cdot d\mathbf{r} = \iint_{S_a} (\nabla \times \mathbf{F}) \cdot \mathbf{n} dS = \pi a^2 (\nabla \times \mathbf{F}) \cdot \mathbf{n}_{av}$$

and taking the limit, we may interpret curl as the limit of the circulation per unit area:

$$(\nabla \times \mathbf{F})_P \cdot \mathbf{n} = \lim_{a \rightarrow 0^+} \frac{1}{\pi a^2} \int_{C_a} \mathbf{F} \cdot \mathbf{T} ds$$

Now consider a small paddle of radius  $a$  and axis  $\mathbf{n}$  rotating with the flow at  $P$ . The approximate angular speed of the paddle  $\omega$  therefore satisfies

$$\begin{aligned} a\omega &= (\mathbf{F} \cdot \mathbf{T})_{av} = \frac{1}{2\pi a} \int_{C_a} \mathbf{F} \cdot \mathbf{n} ds = \frac{\pi a^2}{2\pi a} (\nabla \times \mathbf{F}) \cdot \mathbf{n}_{av} \\ &= \frac{a}{2} (\nabla \times \mathbf{F}) \cdot \mathbf{n}_{av} \end{aligned}$$

Dividing by  $a$  and taking the limits as  $a \rightarrow 0^+$ , we see that an infinitesimal paddle at  $P$  will rotate with angular speed

$$\omega = \frac{1}{2} (\nabla \times \mathbf{F})_P \cdot \mathbf{n} \text{ rad/s}$$

The paddle therefore rotates with maximum velocity if its axis of rotation is parallel to the curl.

